DAYLIGHTING SIMULATION IN DOE-2:
THEORY, VALIDATION, AND APPLICATIONS

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ABSTRACT

A daylighting calculation has been integrated into the DOE-2 building energy analysis computer program. The program allows users to determine the impact of daylight utilization on energy use, energy cost, and peak electrical demand. We describe the algorithms which simulate hourly-varying interior illuminance, management of windows for sun and glare control, and the operation of electric lighting control systems. Sample DOE-2 daylighting output reports are presented, results of program validation against scale model illuminance measurements using the Lawrence Berkeley Laboratory sky simulator are discussed, and some applications of the program are illustrated.

1. INTRODUCTION

A daylighting simulation has been integrated into the DOE-2 building energy use analysis program. This model, in conjunction with the DOE-2 thermal loads and HVAC analysis [1,2], determines the energy- and cost-related consequences of daylighting strategies based upon hour-by-hour analysis of daylight availability, site conditions, window management in response to solar gain and glare, and various lighting control strategies.

The daylighting simulation which is described in the following sections has three main stages:

(1) **Daylight factor preprocessor:** By integrating over the area of each window (or skylight), interior illuminance at user-selected room locations is calculated for a standard overcast sky and for clear sky conditions with 20 different sun positions. Dividing the interior illuminance by the corresponding exterior illuminance gives daylight factors which are stored for later interpolation in the hourly simulation. The interior illuminance calculation accounts for the luminance distribution of the sky; window size, slope and orientation; glass transmittance; inside surface reflectances; sun control devices such as drapes and overhangs; and external obstructions. Analagous factors for the discomfort glare from each window are also calculated for each sun and sky condition and stored.

(2) **Hourly daylighting simulation:** The hourly illuminance and glare contribution from each window is found by interpolating the stored daylight factors using the current-hour sun position and cloud cover, then multiplying by the current-hour exterior horizontal illuminance. If the glare-control option has been specified, the program automatically closes window blinds or drapes in order to decrease glare below a pre-defined comfort level. A similar option uses window shading devices to automatically control solar gain.

This procedure of interpolating pre-calculated daylight factors to obtain hourly illuminance and glare reduces computation time by a factor of 200 compared to hourly re-integration over each window.

(3) **Hourly lighting control simulation:** Stepped and continuously dimming lighting control systems are simulated to determine the electrical lighting energy needed to make up the difference, if any, between the daylighting level and the design illuminance. Finally, the lighting electrical requirements are passed to the thermal calculation which determines hourly heating and cooling requirements for each space and for the building as a whole.

2. DAYLIGHT FACTOR PREPROCESSOR

For each daylit space, the preprocessor calculates a set of daylight factors for a series of sun positions covering the annual range of solar altitude and azimuth at the specified building latitude. These factors relate interior illuminance and glare levels to outdoor daylight levels.

2.1 Interior Illuminance Components

DOE-2 separates daylight incident on a window into two components: (1) sky-related light, i.e., light which originates from the sky, and reaches the window directly or by reflection from exterior surfaces; and (2) sun-related light, i.e., light which originates from the sun, and reaches the window directly or by reflection from exterior surfaces. Light from the window then reaches the workplane directly or via reflection from the interior surfaces of the room. Figure 1a-e shows schematically the various paths by which diffuse light originating from the sky can pass through a window and reach a reference point on the workplane. Figure 1f-j shows similar paths for light originating from the sun.

For a given sun position and sky condition (clear or overcast), the sky-related interior daylight will be proportional to the exterior horizontal illuminance, E_{sky}, due to light from the sky. Similarly, the sun-related interior daylight will be proportional to the exterior horizontal solar illuminance E_s.

2.2 Daylight Factors

The following six ratios (generalized daylight factors) are calculated and stored for later use in the hourly calculation of interior daylight illuminance and window glare:

d_{sky} =(interior illuminance due to sky-related light)/E_{sky}

d_s =(interior illuminance due to sun-related light)/E_s

w_{sky} =(average window luminance due to sky-related light)/E_{sky}

w_s =(average window luminance due to sun-related light)/E_s

b_{sky} =(window surround (background) luminance due to sky-related light)/E_{sky}

b_s =(window surround (background) luminance due to sun-related light)/E_s
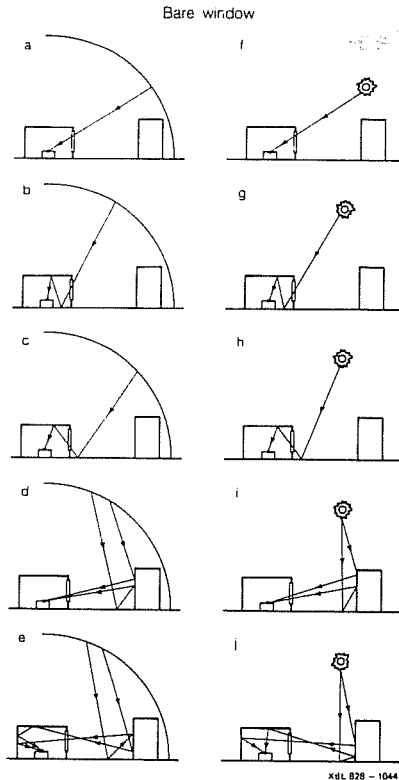
Bare window

Fig. 1.   Paths by which light originating from sky (a-e) and from sun (f-j) can reach workplane through a transparent window without a shading device.

These factors depend on **room conditions**, such as room geometry, surface reflectances, reference point location, window size and orientation, glass transmittance, and window shade transmittance; and on **exterior conditions**, such as ground reflectance, location and reflectance of external obstructions, condition of sky, and position of sun.

The six daylight factors are calculated for each of the following combinations of reference point, window, sky condition, sun position, and shading device:

$$
\begin{bmatrix} \text{Ref pts \#1} \\ \text{(and \#2 if} \\ \text{defined)} \end{bmatrix}
\begin{bmatrix} \text{Window \#1} \\ \text{Window \#2} \\ \cdot \\ \cdot \\ \cdot \\ \text{Window \#N}_w \end{bmatrix}
\begin{bmatrix} \text{Clear sky} \\ \text{sun pos. \#1} \\ \cdot \\ \cdot \\ \cdot \\ \text{Clear sky,} \\ \text{sun pos. \#20} \\ \text{Overcast sky} \end{bmatrix}
\begin{bmatrix} \text{Bare} \\ \text{window} \\ \text{and} \\ \text{Window} \\ \text{plus} \\ \text{shade} \end{bmatrix}
$$

For example, for a room with one reference point, one window, and no window-shade, there are $(1 \times 1 \times 21 \times 1) \times 6 = 126$ daylight factors. In the Northern hemisphere the 20 sun positions for the clear sky case cover a grid of five equally-spaced solar azimuths from 70° to 290° (measured clockwise from North), and four equally-spaced altitudes from 10° (5° for latitudes above 48°) to the maximum altitude reached by the sun at the latitude in question. Figure 2 shows the sun positions for 40° latitude.

2.3 Calculation of Exterior Illuminance

The equations used to calculate exterior illuminance are derived from empirical formulations for standard clear and overcast skies adopted by the Commission Internationale de l'Eclairage (CIE) [3]. These equations are based on the European work of Kittler [4], Krochmann [5], Dogniaux [6], and others.
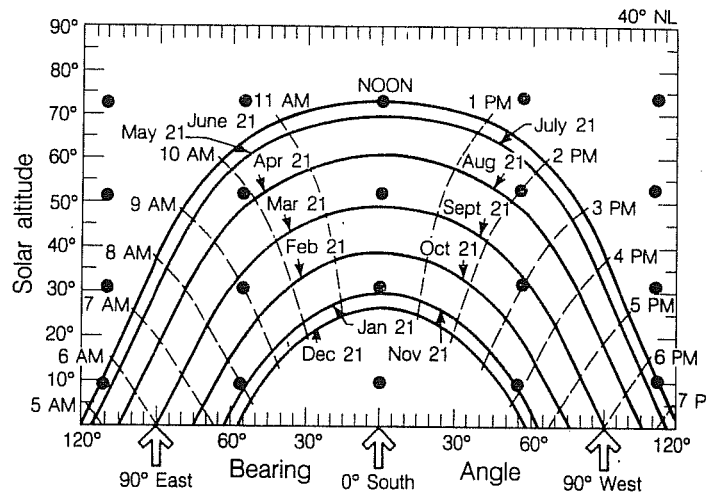

Fig. 2.   Sun positions (•) used by preprocessor for calculation of clear sky daylight factors for 40° north latitude. (Sunchart reproduced from "The Passive Solar Energy Book", Edward Mazria, Rodale Press, Emmaus, PA 1979.)

2.3.1 Direct Solar Illuminance

The horizontal direct solar illuminance at the earth's surface under clear sky conditions can be expressed as [6,7]

$$E_s = E_{DN}^o \, e^{-\overline{a}mT} \, sin\phi_s \tag{1}$$

where E_{DN}^o is the extraterrestrial direct normal illuminance, ϕ_s is the altitude of the sun, m is the optical air mass, T is the atmospheric turbidity, and $\overline{a}$ is an empirically determined atmospheric extinction coefficient. The turbidity is a measure of the aerosol and moisture content of the atmosphere. It has the form [6,7]

$$T = \left[\frac{\phi_{s,deg} + 85}{39.5 \, e^{-w} + 47.4} + 0.1 \right] + (16 + 0.22w) \, \beta \tag{2}$$

where w is the amount of precipitable moisture in the atmosphere [cm of water] and β is Angstrom's turbidity coefficient [8-10]. The value of T ranges from about 2 for a very clean, dry atmosphere, to 5 and above for moist, polluted conditions.

2.3.2 Sky Luminance

Clear sky. The luminance distribution of a clear sky has the form [4,3]

$$L_{cl}(\theta_{sky}, \phi_{sky}) = \tag{3}$$

$$L_{z,cl}(\phi_s) \frac{(0.91 + 10e^{-3\gamma} + 0.45\cos^2\gamma)(1 - e^{-0.32cosec\,\phi_{sky}})}{.27385\,(0.91 + 10e^{-3(\pi/2 - \phi_s)} + 0.45\sin^2\phi_s)}$$

where ϕ_s is the altitude of sun, $L_{z,cl}$ is the zenith luminance of the sky, and γ is the opening angle between sun and sky element. A contour plot of the ratio $L_{cl}(\theta_{sky}, \phi_{sky})/L_{z,cl}$ is shown in Fig. 3 for a solar altitude of 40°. The general characteristics of the distribution are a large peak near the sun; a minimum at a point on the other side of the zenith from the sun; and an increase in luminance as the horizon is approached.
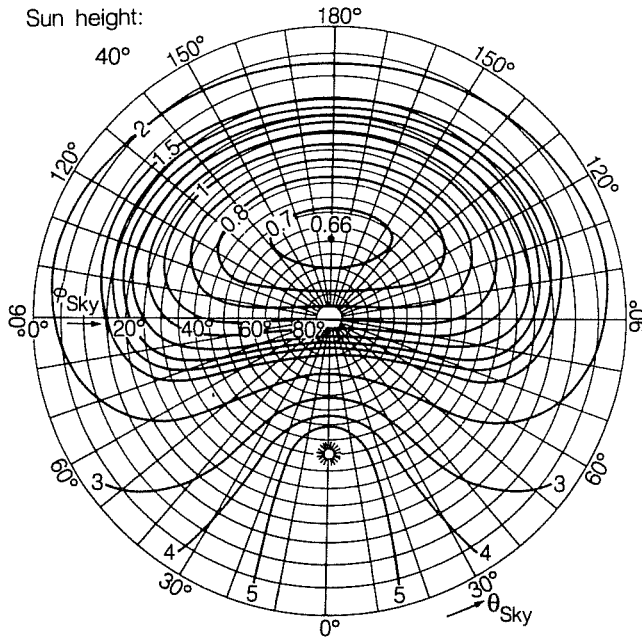
Fig. 3.   Clear sky luminance distribution (normalized to unit zenith luminance) for a solar altitude of 40 °.

The zenith luminance in eqn. (3) is given by [11]

$$L_{z,cl}[kcd/m^2]=(1.34T-3.46)\tan\phi_s+0.10T+0.90, \phi_s \leq 60/(de \quad (4)$$

and $T>3$.

For $\phi_s > 60$ °, where eqn. (4) is invalid, $L_{z,cl}$ is taken to be

$$L_{z,cl}(\phi_s)= \quad (5)$$

$$\frac{3.25L_{z,cl}(60°)\sin\phi_s}{[3.25-.1050(\phi_s-60)+.0010(\phi_s-60)^2]\sin60°}, \phi_s > 60°,$$

which was obtained [12] by constraining the horizontal illuminance to increase as $\sin\phi_s$ for $\phi_s > 60$ °. For values of T less than 3, eqn. (4) is used with $T=3$.

Overcast sky. The CIE standard overcast sky luminance distribution has the form [13]

$$L_{oc}(\phi_{sky}) = L_{z,oc}\frac{1+2\sin\phi_{sky}}{3}, \quad (6)$$

where the zenith luminance, $L_{z,oc}$, is [5]

$$L_{z,oc}[kcd/m^2] = 0.123 + 8.6\sin\phi_s . \quad (7)$$

The overcast sky luminance distribution, unlike the clear sky case, does not depend on either the solar azimuth or the sky azimuth. The zenith is three times brighter than the horizon.

2.3.3 Luminous Efficacy of Solar Radiation

If measured solar irradiance values are present on the DOE-2 weather file, the luminous efficacy in lumens/watt is calculated for direct solar radiation, clear sky diffuse solar radiation, and overcast sky diffuse solar radiation. These efficacies, multiplied by solar irradiance, are used to obtain hourly exterior illuminance values, as described below in Section 3.1.

Direct Solar Radiation. The luminous efficacy of direct solar radiation as parameterized by Dogniaux [6,7] is

$$K_s [lm/W] = K_o e^{-mT(\bar{a}-\bar{a}_s)} \quad (8)$$

where K_o is the extraterrestrial luminous efficacy (93.73 lm/W) and $\bar{a}_s$ is the atmospheric extinction coefficient due to Rayleigh scattering of solar radiation.

K_s is plotted as a function of solar altitude for high and low values of atmospheric moisture, w, and decadic turbidity factor, $B(B \approx 1.07\beta)$ in Fig. 4. The rapid fall-off in K_s for $\phi_s < 30$ ° is primarily due to the λ^{-4} wavelength dependence of Rayleigh scattering. K_s increases with w since the absorption of solar radiation by atmospheric water vapor is much higher in the infrared than the visible.

Diffuse Solar Radiation. The luminous efficacy, K_{cl}, of clear sky diffuse radiation as a function of B, w, and solar altitude is shown in Fig. 5, which is based on theoretical calculations by Aydinli [14,15]. K_{cl} varies from 115 to 135 lm/W, with a mean value of 125.4 lm/W and standard deviation of 6.1 lm/W. Because of the relatively small standard deviation in $K_{cl}(\pm5\%)$, the mean value of K_{cl} is used in DOE-2.

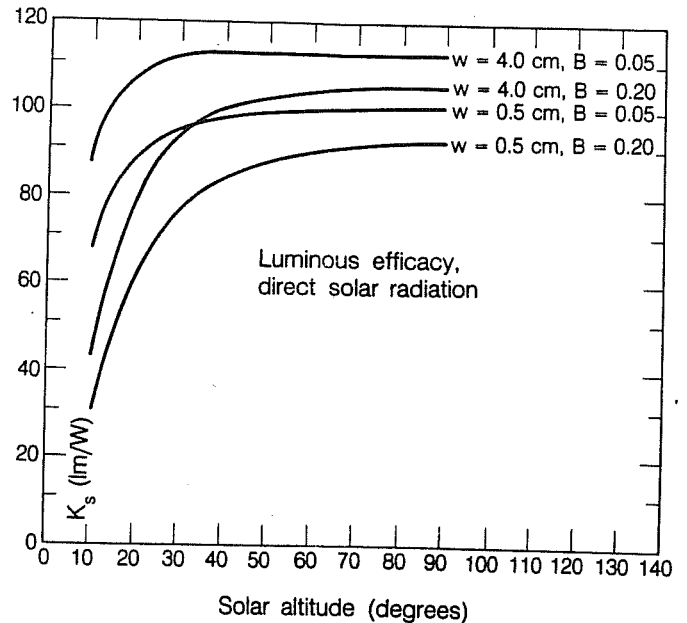Fig. 4.   Luminous efficacy of direct solar radiation for selected values of atmospheric moisture, w, and decadic turbidity coefficient, $B(B =1.07\beta)$.
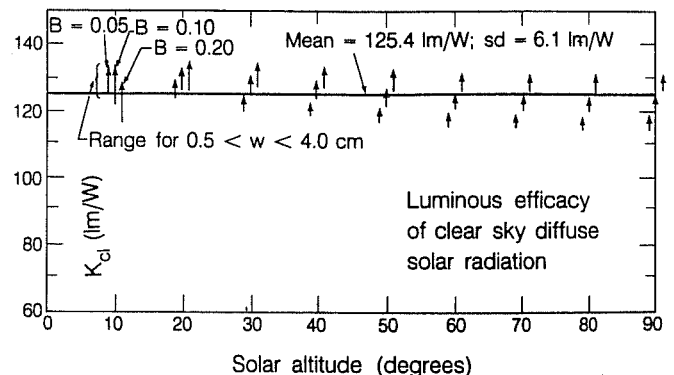
2.4 Calculation of Interior Illuminance

2.4.1 Direct Component

The direct daylight illuminance E_d from a window is determined by dividing the window into an x-y grid and finding the flux reaching the reference point directly (i.e., without interior reflection) from each grid element. The net direct horizontal illuminance from the window is the sum of the contributions from all the window elements which lie above the workplane:

$$E_d = \sum L_w \, d\omega \, \cos\psi \,, \tag{9}$$

where L_w is the luminance of the window element as seen from the reference point, $d\omega$ is the solid angle subtended by the window element with respect to the reference point, and ψ is the angle between the vertical and the ray from the reference point to center of the window element.

Bare Window. For the bare window case, the luminance L_w of the window element is found by projecting the ray from reference point to window element and determining whether it intersects the sky or an exterior obstruction. It is assumed that there are no internal obstructions. If L is the corresponding luminance of sky or exterior obstruction, the window luminance is $L T_g(\eta)$, where T_g is the visible transmittance of the glass for incidence angle η.

Window with Shade. For the window-plus-shade case, the shade is assumed to be a perfect diffuser, i.e., the luminance of the shade, L_{sh}, is independent of angle of emission of light, position on shade, and angle of incidence of exterior light falling on the shade. The illuminance contribution at the reference point from a shade element is given by eqn. (9) with $L_w = L_{sh}$ if the shade is inside the window, or $L_w = L_{sh} T_g(\eta')$ if the shade is outside the window, where η' is the angle of emission of light from the shade.

2.4.2 Internally reflected component

Daylight reaching a reference point after reflection from interior surfaces is calculated using the "split-flux" method [16,17]. The daylight transmitted by the window is split into two parts -- a downward-going flux, Φ_{FW} [lm], which falls on the floor and portions of the walls below the imaginary horizontal plane passing through the center of the window "window midplane"), and an upward-going flux Φ_{CW} [lm], which strikes the ceiling and portions of the walls above the window midplane (see Fig. 6).
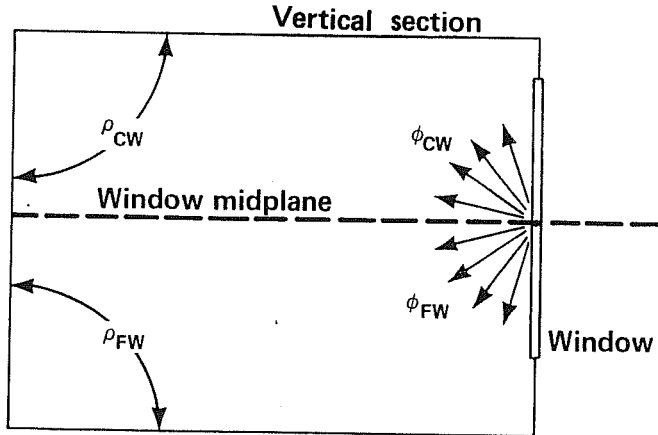
Vertical section

Fig. 6. Vertical section showing up- and down-going transmitted fluxes, ϕ_{CW} and ϕ_{FW}, used in split-flux calculation of the internally-reflected component of interior illuminance.

A flux balance gives the final average internally-reflected illuminance E_r (which in this method is uniform throughout the room):

$$E_r \; [lm/unit\text{-}area] = \frac{\Phi_{FW} \, \rho_{FW} + \Phi_{CW} \, \rho_{CW}}{A \, (1-\rho)}, \tag{10}$$

where ρ_{FW} is the area-weighted average reflectance of the floor and those parts of the walls below the window mid-plane, and ρ_{CW} is the area-weighted average reflectance of the ceiling and those parts of the walls above the window mid-plane, A is the total inside surface area of the room, and ρ is the area-weighted average inside surface reflectance.

This procedure assumes that the room behaves like an integrating sphere with perfectly diffusing interior surfaces and no internal obstructions. It therefore works best for rooms which are close to cubical in shape, have matte surfaces (which is usually the case), and have no internal partitions. For these reasons, the split-flux method is not recommended for rooms whose depth measured from the window-wall is more than approximately three times greater than ceiling height; in this case the method can overpredict the internally-reflected illuminance near the back of the room by a factor of two or more (see Section 6 and Fig. 9c-f).

Transmitted Flux From Sky and Ground. The luminous flux incident on the center of the window from a luminous element of sky, ground, or external obstruction at angular position (θ,ϕ), of luminance $L(\theta,\phi)$, and subtending a solid angle $\cos\phi \, d\theta \, d\phi$ is

$$d\Phi_{inc} = A_W \, L(\theta,\phi) \, \cos\eta \, \cos\phi \, d\theta \, d\phi \tag{11}$$

where A_W is the window area, and $d\Phi_{inc}$ is in lm if L is in cd/unit-area. The transmitted flux is

$$d\Phi = d\Phi_{inc} \, T_w$$

where T_w is the window transmittance. If $T_g(\eta)$ is the glass transmittance for incidence angle η, $T_{g,dif}$ is the glass transmittance for diffuse illuminance, and T_{sh} is the shade transmittance, then

$$T_w = T_g(\eta) \text{ for unshaded glass,}$$
$$= T_g(\eta) T_{sh} \text{ for glass with inside shading device,}$$
$$= T_{sh} T_{g,dif} \text{ for glass with outside shading device.}$$

For a bare window of arbitrary tilt the total downgoing transmitted flux, Φ_{FW}, is obtained by integrating $d\Phi$ over the part of the exterior hemisphere seen by the window which lies above the window midplane. This gives

$$\Phi_{FW,bare} = A_w \int_0^{\pi/2} d\phi \int_{-\theta_{max}}^{\theta_{max}} L(\theta,\phi) \, \cos\eta \, T_g(\eta) \, \cos\phi \, d\theta \tag{12}$$

where, if ϕ_w is the altitude angle of the outward normal to the window, $\theta_{max} = |\cos^{-1}(-\tan\phi \, \tan\phi_w)|$ (see ref. 12).

The upgoing flux, $\Phi_{CW,bare}$, is similarly obtained by integrating over the part of the exterior hemisphere which lies below the window midplane:

$$\Phi_{CW,bare} = A_w \int_{\pi/2-\phi_w}^{0} d\phi \int_{-\theta_{max}}^{\theta_{max}} L(\theta,\phi) \, \cos\eta \, T_g(\eta) \, \cos\phi \, d\theta \tag{13}$$

For a window with a diffusing shade, the total transmitted flux is first calculated:

$$\Phi = A_w \int_{\pi/2-\phi_w}^{\pi/2} d\phi \int_{-\theta_{max}}^{\theta_{max}} L(\theta,\phi) \cos\eta \, T_w(\eta) \cos\phi \, d\theta \quad (14)$$

This is then divided into up- and down-going portions given, respectively, by $\Phi_{FW,sh} = \Phi(1-f)$ and $\Phi_{CW,sh} = \Phi f$, where f is the fraction of the hemisphere seen by the inside of the window which lies above the window midplane. For a vertical window, $f = 0.5$, and the up- and down-going transmitted fluxes are equal: $\Phi_{FW,sh} = \Phi_{CW,sh} = \Phi/2$. For a horizontal skylight, $f = 0$, giving $\Phi_{FW,sh} = \Phi$ and $\Phi_{CW,sh} = 0$.

Flux From Sun. The incident luminous flux from direct sun striking the window at incidence angle η is

$$\Phi_{inc} = A_w E_{DN} \cos\eta \, (1-f_{shaded}) \, , \; \cos\eta \geq 0 \quad (15)$$
$$= 0 \, , \; \cos\eta < 0 \, ,$$

where E_{DN} is the direct normal solar illuminance and f_{shaded} is the fraction of window which is shaded by obstructions such as fins, overhangs, or neighboring buildings.

The transmitted flux is $\Phi = T_w(\eta)\Phi_{inc}$. For a bare window, $\Phi_{FW,bare} = \Phi$ and $\Phi_{CW,bare} = 0$, i.e., all of the transmitted flux is downward since the sun always lies above the window midplane. For a window with a diffusing shade, $\Phi_{FW,sh} = \Phi(1-f)$ and $\Phi_{CW,sh} = \Phi f$.

Window Shade Luminance. The window shade luminance is determined at the same time that the transmitted flux is calculated. It is given by

$$L_{sh} = \frac{1}{\pi} \int_{\pi/2-\phi_w}^{\pi/2} d\phi \int_{\theta_{min}}^{\theta_{max}} L(\theta,\phi) \cos\eta \, T_m \cos\phi \, d\theta \quad (16)$$

where T_m is equal to T_{sh} for an outside shade and is equal to $T_g(\eta) \, T_{sh}$ for an inside shade.

2.5 Calculation of Discomfort Glare from Windows

Since discomfort glare is subjective, it is difficult to quantify and the reliability of existing parameterizations is controversial [18]. For DOE-2, we have chosen the formulation of Hopkinson [19,20] as being the best available at the present time. In this formulation the discomfort glare at a reference point due to luminance contrast between a window and the interior surfaces surrounding the window is given by

$$G = \frac{0.48 \, L_w^{1.6} \, \Omega^{0.8}}{L_b + 0.07 \, \omega^{0.5} \, L_w} \quad (17)$$

where G is the discomfort glare constant, L_w is the average luminance of the window as seen from the reference point (cd/m^2), ω is the solid angle subtended by the window with respect to reference point, Ω is the solid angle subtended by the window and modified to take direction of occupant view into account, and L_b is the average luminance of the background area surrounding the window (cd/m^2).

Dividing the window into N_x by N_y rectangular elements, as is done for calculating the direct component of interior illuminance, gives

$$L_w = \frac{1}{N_x N_y} \sum_{j=1}^{N_y} \sum_{i=1}^{N_x} L_w(i,j) \quad (18)$$

where $L_w(i,j)$ is the luminance of element (i,j) as seen from the reference point.

The background luminance is given by $L_b = E_b \rho_b$, where E_b is the average illuminance on the floor, wall, and ceiling surfaces surrounding the window; ρ_b is the average reflectance of these surfaces. In DOE-2, ρ_b is approximated by the average interior surface reflectance, ρ, of the entire room. E_b is approximated by the larger of E_d and E_{set}, where E_r is the total internally-reflected component of daylight illuminance produced by all the windows in the room; E_{set} is the illuminance setpoint at the reference point at which glare is being calculated. A precise calculation of L_b is not required since the glare index (described below) is logarithmic: a factor of two variation in L_b generally produces a change of less than 1.0 in the glare index.

The net daylight glare at a reference point due to all of the windows in a room is expressed in terms of a glare index, GI, which is given by

$$GI = 10\log_{10} \sum_{i=1}^{N_W} G_i \quad (19)$$

where G_i is the glare constant at the reference point due to the ith window. The recommended maximum allowable values of GI depend on space function. Typical values are 18 for hospital wards, 20 for school classrooms and drafting, and 22 for general office work [22].

The glare formulation used in DOE-2 does not account for glare caused by penetration of beam radiation into a room through unshaded windows. However, admittance of direct solar gain in spaces requiring good visual performance is usually not good design practice. Therefore, windows lacking fixed architectural elements such as fins or overhangs to block direct sun would normally have operable shading systems (e.g. shades, blinds, draperies) to control direct sun when it is present. Deployment of these devices can be simulated in DOE-2 using the window management option with a user-defined direct solar gain setpoint. The program then calculates the transmitted radiation through the unshaded window each hour and deploys the shading device whenever the transmitted radiation exceeds the trigger level.

3. HOURLY DAYLIGHTING CALCULATION

A daylighting calculation is performed each hour that the sun is up. The exterior horizontal illuminance from sun and sky is calculated theoretically for the current-hour sun position and cloud amount, or is determined from solar irradiance data if present on the weather file. The interior illuminance at each reference point is found for each window by interpolating the illuminance factors calculated by the preprocessor. By summation, the net illuminance and glare due to all the windows in a space are found. If glare or solar gain exceed user-specified thresholds, window shading devices can be deployed. The daylight illuminance at each reference point for the final window-shade configuration is used by the lighting control system simulation to determine the electric lighting power required to meet the illuminance setpoint.

3.1 Hourly Exterior Daylight Availability

For the current-hour sun position and current-month atmospheric moisture and turbidity, eqns. (3) and (6) are used to obtain the exterior horizontal illuminance from a standard clear sky (E_{cl}) and from a standard overcast sky (E_{oc}). If the weather file has solar irradiance data, the program finds the current-hour luminous efficacy, K_s, for standard clear sky direct solar radiation using eqn. (8).

Because few data exist on the luminous characteristics of partly-cloudy skies, we have made the simplifying assumption that the sky in a given hour can be divided into a uniformly distributed fraction, η_{cl}, which has the clear sky luminance distribution for the current sun position, and a fraction $\eta_{oc} = 1-\eta_{cl}$ which has the overcast sky luminance distribution. η_{cl} is taken to be a function of CR, the

fraction of the skydome covered with clouds (obtained from the weather file). The form chosen for η_{cl} vs CR, shown in Fig. 7, gives a clear sky luminance distribution for the whole sky for $CR \leq 0.2$. As CR increases above 0.2, the average cloud luminance is assumed to become progressively closer to the standard overcast sky luminance.
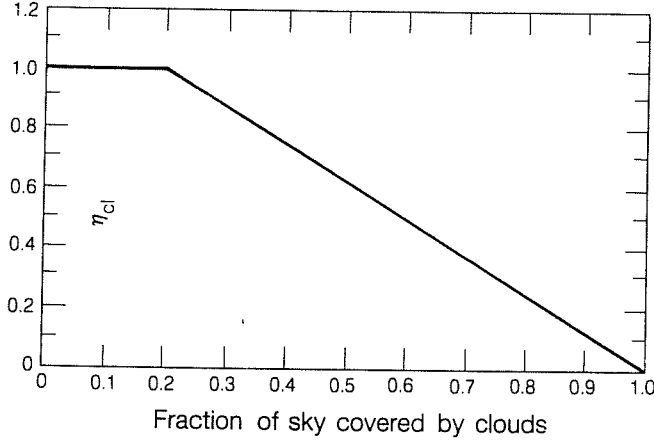
Fig. 7.   Effective fraction of sky, η_{cl}, having standard clear sky luminous distribution vs fraction of sky covered by clouds. The remainder of the sky, $1-\eta_{cl}$, is assumed to have a standard overcast sky luminance distribution.

The average exterior horizontal illuminance due to the fraction of sky with standard clear sky characteristics is then $\eta_{cl}E_{cl}$. Correspondingly, $\eta_{oc}E_{oc}$ is the exterior horizontal illuminance due to the fraction of sky with standard overcast sky characteristics. The average direct solar exterior horizontal illuminance for the current hour is taken to be

$$\overline{E}_s = (1-CR)\, E_s \; , \tag{20}$$

where E_s, the clear-sky solar illuminance, is obtained from eqn. (1).

If the weather file has measured solar radiation data, this expression is replaced by

$$\overline{E}_s = K_s \, I_{DN}^{meas} \, \sin\phi_s \; , \tag{21}$$

where K_s is the luminous efficacy [lm/W] of solar radiation from eqn. (13), and I_{DN}^{meas} is the measured direct normal solar irradiance [W/m^2]. In addition, the horizontal illuminance values from the clear and overcast portions of the sky are each adjusted by a multiplicative factor α so that their sum equals the measured horizontal diffuse irradiance, I_d^{meas}, times the luminous efficacy. The quantity α is thus obtained from

$$\alpha \left(\eta_{cl}E_{cl} + \eta_{oc}E_{oc}\right) = I_d^{meas} \left(\eta_{cl}K_{cl} + \eta_{oc}K_{oc}\right) \tag{22}$$

3.2 Hourly Workplane Illuminance and Window Background Luminance

The hourly average workplane illuminance at a reference point is given by

$$E = \sum_{i=1}^{N_w} \left[d_s(i,i_{sh})E_s + d_{cl}(i,i_{sh})\eta_{cl}E_{cl} + d_{oc}(i,i_{sh})\eta_{oc}E_{oc} \right] \tag{23}$$

where i is the window index; i_{sh} is 1 for open shade and 2 for closed shade; and d_s, d_{cl}, d_{oc} are daylight factors for sun-related, clear-sky-related, and overcast-sky-related illuminance, respectively. The values

of d_s and d_{cl} depend on the current-hour sun position. They are obtained by linearly interpolating, in solar altitude and azimuth, the corresponding daylight factors calculated by the preprocessor.

The current-hour background luminance of a window is, similarly,

$$L_b = b_s(i,i_{sh})E_s + b_{cl}(i,i_{sh})\eta_{cl}E_{cl} + b_{oc}(i,i_{sh})\eta_{oc}E_{oc}, \tag{24}$$

where b_s, b_{cl} and b_{oc} are the interpolated daylight factors for background luminance.

The current-hour average luminance of a window is

$$L_{w,i} = w_s(i,i_{sh})E_s + w_{cl}(i,i_{sh})\eta_{cl}E_{cl} + w_{oc}(i,i_{sh})\eta_{oc}E_{oc} \tag{25}$$

where w_s, w_{cl} and w_{oc} are the interpolated daylight factors for window luminance.

3.3 Hourly Glare Index

From eqns. (26) and (30), the current-hour glare index at a reference point is

$$GI = 10\log_{10} \sum_{i=1}^{N_w} \frac{0.48\, L_{w,i}^{1.6}\, \Omega_i^{0.8}}{L_b' + 0.07\, \omega_i^{0.5}\, L_{w,i}}, \tag{26}$$

where L_b' is the larger of the window surround luminance, L_b, from daylight, and the average surround luminance which would be produced by the electric lighting at full power if the illuminance on the room surfaces were equal to the setpoint illuminance.

3.4 Glare Control Simulation

If the glare index at either reference point exceeds a user-specified threshold value, GI_{max}, shading devices are closed sequentially until the glare index at both points is below GI_{max}. Each time a shading device is closed, the glare index and illuminance at each reference point are recalculated.

3.5 Electric Lighting Control System Simulation

In DOE-2, the user can divide a room into one or two lighting zones. The electric lighting power in each zone is assumed to be controlled by a sensor which responds to the illuminance at the user-specified reference point for that zone. If the daylight illuminance at a reference point is E, the fractional electric light output required to meet a design illuminance value, E_{set}, is

$$f_L = (E_{set} - E)\, / \, E_{set} \; , \quad E < E_{set} \tag{27}$$
$$= 0 \; , \quad E \geq E_{set}$$

For a continuously dimmable control system, the lighting power curve is assumed to be linear in fractional electrical input power, f_p, vs. f_L. For a stepped control system, f_p takes on discrete values depending on the number of steps.

4. FUNCTIONAL VALUE INPUT

A new feature introduced in the DOE-2.1C version of the program allows users to modify the daylighting and thermal loads calculation algorithms by entering FORTRAN-like functions in the program input. This "functional input" capability permits analysis of innovative design alternatives which previously would have required difficult and time-consuming alteration and recompilation of DOE-2 subroutines. Some daylighting-related applications of functional input are as follows:

(1) The user can input daylight factors obtained from scale model photometric measurements. The program would then use these factors instead of the internally calculated values to determine hourly illuminance. This allows DOE-2 to be used for energy analysis of arbitrarily complex daylighting situations.

(2) Advanced glazing materials can be modeled. Examples are angle-selective glazing (with transmittance vs. angle of incidence radically different from the default transmission curves in DOE-2) and glazing whose transmittance is actively or passively controlled by

a

REPORT LS-C SPACE DAYLIGHTING SUMMARY   WEATHER FILE -- MADISON, WI WYEC

SPACE SOUTHZONE

------------------ REPORT SCHEDULE HOURS WITH SUN UP ------------------

MONTH	PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (ALL HOURS)			PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (REPORT SCHEDULE HOURS)			AVERAGE DAYLIGHT ILLUMINANCE (LUX)		PERCENT HOURS DAYLIGHT ILLUMINANCE ABOVE SETPOINT		AVERAGE GLARE INDEX		PERCENT HOURS GLARE TOO HIGH	
	TOTAL ZONE	REF PT 1	REF PT 2	TOTAL ZONE	REF PT 1	REF PT 2	REF PT 1	REF PT 2	REF PT 1	REF PT 2	REF PT 1	REF PT 2	REF PT 1	REF PT 2
JAN	28.2	34.8	21.7	36.5	45.0	28.0	371.8	173.6	23.7	0.7	19.0	17.2	23.7	17.9
MAR	37.9	45.8	29.9	47.3	56.8	37.8	501.7	241.7	41.2	3.2	20.8	19.4	41.2	30.1
MAY	35.4	46.3	24.4	41.9	54.5	29.3	373.9	183.6	13.6	0.0	20.0	18.6	12.9	1.8
JUL	37.1	48.9	25.2	44.0	57.8	30.2	383.1	188.3	7.9	0.0	20.3	18.9	6.5	0.0
SEP	38.4	47.1	29.7	46.9	57.0	36.7	484.6	237.0	41.5	0.4	20.9	19.7	41.5	28.5
NOV	26.5	33.1	19.8	34.1	42.5	25.6	374.2	173.1	24.8	0.7	18.2	16.5	24.8	21.5
ANNUAL	33.9	42.6	25.1	41.7	52.2	31.3	411.8	198.0	25.9	0.8	19.8	18.3	25.5	16.9

b

REPORT LS-H PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHT   WEATHER FILE -- MADISON, WI WYEC

SPACE SOUTHZONE

HOUR OF DAY

MONTH	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	ALL HOURS
JAN	0	0	0	0	0	0	0	3	20	38	47	50	49	50	42	25	10	0	0	0	0	0	0	0	28
MAR	0	0	0	0	0	0	6	24	41	50	47	54	54	50	49	49	32	14	0	0	0	0	0	0	38
MAY	0	0	0	0	0	19	27	35	38	41	44	44	45	47	43	40	32	22	10	0	0	0	0	0	35
JUL	0	0	0	0	0	14	21	29	43	43	45	48	51	50	46	43	28	25	20	1	0	0	0	0	37
SEP	0	0	0	0	0	0	19	34	45	46	51	53	53	51	48	43	32	11	0	0	0	0	0	0	38
NOV	0	0	0	0	0	0	0	12	30	42	47	49	47	42	34	17	2	0	0	0	0	0	0	0	26
ANNUAL	0	0	0	0	0	7	17	29	37	43	47	50	50	47	43	36	20	10	5	0	0	0	0	0	34

c

REPORT LS-J DAYLIGHT ILLUMINANCE FREQUENCY OF OCCURRENCE   WEATHER FILE -- MADISON, WI WYEC

SPACE SOUTHZONE

PERCENT OF HOURS IN ILLUMINANCE RANGE   PERCENT OF HOURS ILLUMINANCE LEVEL EXCEEDED

MONTH	REF PT	ILLUMINANCE RANGE (LUX) 0--100	100--200	200--300	300--400	400--500	500--600	600--700	700--800	800--ABOVE	ILLUMINANCE LEVEL (LUX) 0	100	200	300	400	500	600	700	800
JAN	-1-	13	25	20	10	8	5	3	4	12	100	87	62	42	32	24	18	15	12
	-2-	47	23	12	6	11	1	0	0	0	100	53	30	18	12	1	0	0	0
MAR	-1-	3	15	15	15	11	11	8	9	14	100	97	82	67	52	41	30	22	14
	-2-	23	27	21	16	10	3·	0	0	0	100	77	51	29	14	3	0	0	0
MAY	-1-	0	21	15	26	24	12	2	0	0	100	100	79	64	38	14	2	0	0
	-2-	23	42	33	3	0	0	0	0	0	100	77	36	3	0	0	0	0	0
JUL	-1-	0	9	22	30	32	7	1	0	0	100	100	91	69	39	8	1	0	0
	-2-	11	53	34	3	0	0	0	0	0	100	89	37	3	0	0	0	0	0
SEP	-1-	0	18	14	13	14	13	14	9	7	100	100	82	69	55	41	29	15	7
	-2-	23	23	25	23	6	0	0	0	0	100	77	54	29	6	0	0	0	0
NOV	-1-	18	20	17	14	6	3	5	7	10	100	82	62	45	30	25	22	17	10
	-2-	44	25	9	12	9	1	0	0	0	100	56	30	21	10	1	0	0	0
ANNUAL	-1-	6	18	18	18	14	9	6	5	6	100	94	76	58	40	26	17	11	6
	-2-	29	32	21	11	5	1	0	0	0	100	71	39	17	6	1	0	0	0

d

HOURLY-REPORT

MMDDHH	GLOBAL CLOUD AMOUNT	GLOBAL SOLAR ALTITUDE DEGREES	GLOBAL SOLAR AZIMUTH DEGREES	GLOBAL EXT ILL CLR SKY LUX	GLOBAL EXT ILL OVR SKY LUX	SOUTHWIN SHADING FLAG	SOUTHZON DAYL ILL REF PT 1 LUX	SOUTHZON DAYL ILL REF PT 2 LUX	SOUTHZON GLR INDX REF PT 1	SOUTHZON LTPW MUL REF PT 1	SOUTHZON LTPW MUL REF PT 2	SOUTHZON LTPW MUL TOTAL
4 2 6	9.0	1.5	85.0	217.	117.	1.	10.5	3.5	1.3	1.00	1.00	1.00
4 2 7	10.0	8.5	91.6	0.	4752.	1.	93.7	33.9	14.2	0.85	0.94	0.90
4 2 8	10.0	19.3	102.2	0.	11561.	1.	228.0	82.5	18.9	0.63	0.87	0.75
4 2 9	9.0	29.7	114.0	5299.	19784.	2.	201.3	100.1	17.4	0.67	0.84	0.76
4 210	7.0	39.1	128.2	12455.	12851.	2.	478.6	237.7	21.5	0.30	0.61	0.46
4 211	4.0	46.6	145.9	14392.	3322.	2.	665.8	330.5	22.9	0.30	0.46	0.38
4 212	7.0	50.9	167.7	8864.	10618.	2.	695.8	345.3	23.1	0.30	0.44	0.37
4 213	8.0	51.0	191.6	10950.	23623.	2.	541.9	269.9	22.1	0.30	0.56	0.43
4 214	10.0	46.8	213.5	0.	36967.	2.	269.9	134.3	18.9	0.56	0.78	0.67
4 215	10.0	39.4	231.3	0.	11917.	1.	235.0	85.1	19.1	0.62	0.86	0.74
4 216	10.0	30.0	245.6	0.	18205.	1.	362.6	133.6	22.1	0.41	0.78	0.60
4 217	10.0	19.7	257.5	0.	11210.	1.	221.1	80.0	18.8	0.64	0.87	0.76
4 218	10.0	8.8	268.1	0.	2081.	1.	41.0	14.9	9.1	0.93	0.98	0.95

Fig. 8. Sample DOE-2 daylighting program reports for the south-facing office module described in text. Selected months only are shown in (a)-(c). Quantities under "REPORT SCHEDULE HOURS" in (a) are restricted to a user-selected time period 8:00am to 5:00pm, the hours of major occupancy. The hourly report in (d) is for sun-up hours on April 2; in this example "CLOUD AMOUNT" is the fraction of sky covered by clouds, in tenths; "EXT ILL CLR SKY" and "EXT ILL OVR SKY" are the exterior horizontal illuminance from the clear and overcast sky portions of the sky, respectively; "SHADING FLAG" is 1 if window drapes are open, 2 if closed; "LTPW MUL" is the multiplier on electric lighting power due to dimming of lights.

environmental conditions such as glass temperature or incident solar radiation intensity.

(3) Complex lighting control schemes can be simulated, including non-linear dimming systems.

(4) The algorithms used to calculate exterior daylight availability can be modified to conform to latest research results on luminous efficacy, partly-cloudy sky luminance distributions, etc.

5. DAYLIGHTING OUTPUT REPORTS

The value of energy simulation studies can be limited or enhanced by the quality and quantity of output data available to the program user. In order to determine the real value of daylighting as an energy conservation strategy, it is essential to understand not only the energy savings, but also the time-varying patterns of daylight utilization within each space. We have provided a series of new reports that provide different levels of information on daylighting performance. Careful analysis and interpretation of these reports can speed the process of arriving at a building design that meets required performance criteria. Figure 8 shows four sample daylighting reports for a south-facing office module using a weather file (with measured solar radiation data) for Madison, Wisconsin. The module is 6.1m wide, 9.2m deep, and is 3.0m floor-to-ceiling. It has a 1.5m high strip window with 0.9m sill height and 90% transmittance. Drapes with 35% transmittance are assumed to be closed by occupants if direct solar transmission exceeds 63 W/m^2 (20 Btu/ft^2-hr) or if glare is excessive ($GI > 22$). There are two independently-controlled lighting zones (each 4.6m deep) with reference points 3.0m and 7.6m respectively from the window-wall, and with design illuminance of 538 lx (50 fc). Each lighting zone has a continuously dimmable control system, which dims linearly to 20% light output at 30% input power.

Figure 8a provides the type of monthly and annual summary data useful in estimating the savings and cost-effectiveness of a daylighting strategy. Figure 8b provides details of the hourly/monthly pattern of lighting energy savings. These results can be printed zone by zone and for the entire building. A frequently observed pattern is one in which savings are maximized at midday, but early morning and late afternoon values are well below maximum. Adding glazing in these cases will save little extra lighting energy and may significantly increase cooling loads. Figure 8c gives statistics on the frequency of occurrence of various interior daylight illuminance values and on the cumulative probability of exceeding each value. Without rerunning the DOE-2 program, the user can estimate the change in daylighting savings if a design illuminance value is changed or the lighting control strategy is altered.

Figure 8d shows an example of a report with hourly values of daylighting-related variables for a particular day. The quantities appearing in this type of report are selected by the user from a list of about 200 different thermal and daylighting variables. The user also selects the time periods the report is printed, allowing, for example, hourly daylighting profiles to be made for typical days at different times of the year.

6. VALIDATION

Two types of validation studies have been undertaken: (1) Parametric analyses have been done to test the sensitivity of each calculation process to key design parameters. For example, the influence of window size, window transmittance, and interior surface reflectance has been examined under a variety of sun and sky conditions. (2) A three-way comparison has been made among DOE-2, SUPERLITE (a detailed illuminance calculation program [23]), and illuminance measurements made in scale models in the Lawrence Berkeley Laboratory sky simulator [24]. Representative results for clear and overcast conditions for a small, single-occupant office model and a deep open-landscape office model are shown in Fig. 9. The difference in the ratio of the three methods is generally ≤15% except very near the window (where the illuminance is not of particular interest) and far from the window-wall in the deep model (Fig. 9c-f) where the split-flux method used in DOE-2 overpredicts the inter-reflected illuminance.
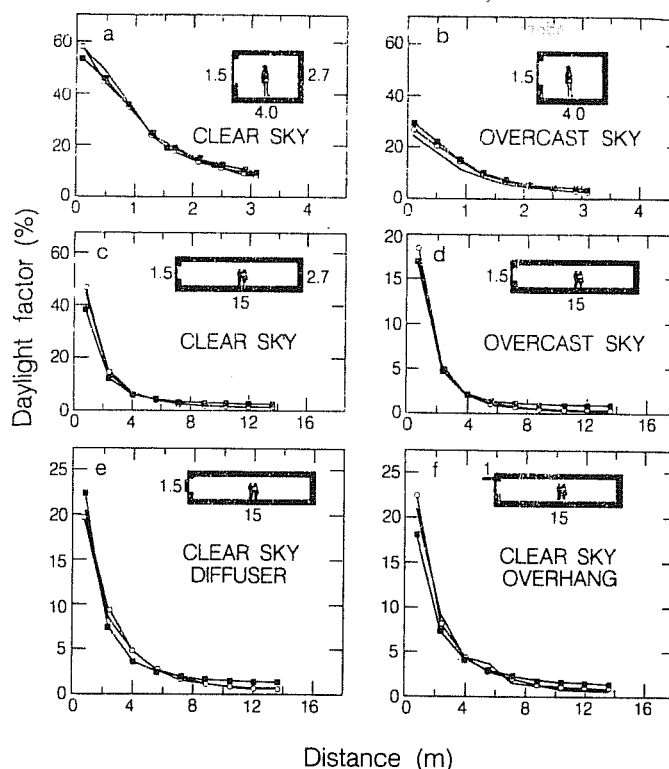

Fig. 9.   (a)-(f): SUPERLITE (O) and DOE-2 (□) predictions for interior/exterior illuminance ratio compared with sky-simulator measurements (-) made along centerline of different scale models. Cases of clear sky have solar altitude 50°, azimuth 0°, but exclude direct sun. Ground reflectance is zero. Interior reflectances are 25% for floor, 60% for walls, 80% for ceiling. Glass transmittance is 90%; diffuser transmittance in (e) is 60%.

7. APPLICATIONS

The DOE-2 program, with its integrated daylighting simulation, has a wide range of design applications. Typical questions which the program can answer are:

(1) What combination of glass area and transmittance will maximize the cost or energy saving benefits of daylighting? An example of the trends to be expected are given in Fig. 10. Shown are DOE-2 predictions for total annual energy use with and without daylighting for a sidelit, south-facing office module in Los Angeles [25]. The parameters being varied are effective aperture, α_{eff} (window-to-wall ratio times visible transmittance) and lighting power density. (Results of this kind can be obtained in DOE-2 in a single run using the PARAMETRIC-INPUT feature.) As α_{eff} increases from zero, we observe that the curves with daylighting controls fall initially due to reduced electric lighting energy, then rise with increasing cooling load from solar gain.

(2) What are the effects of daylighting with skylights? Figure 11, for example, shows DOE-2 predictions for energy use vs α_{eff} for a skylit top floor of an office building in Los Angeles [26]. One conclusion in this case is that minimum energy use occurs at much smaller values of α_{eff} than for the sidelit situation in Fig. 10.

(3) What are the relative impacts of stepped switching vs continuous dimming of electric lights? A typical result is shown in Fig. 12 which gives a DOE-2 comparison of these two control methods for a south-facing office module in Madison, WI [27]. In this example we see that continuous dimming is preferable for effective apertures up to 0.3.

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SIDELIGHTING

NO DAYLIGHTING CONTROLS
CONTINUOUS DIMMING

Total energy consumption — MBTU/yr vs effective aperture — WWR × VT

1 2.7 watts/sf
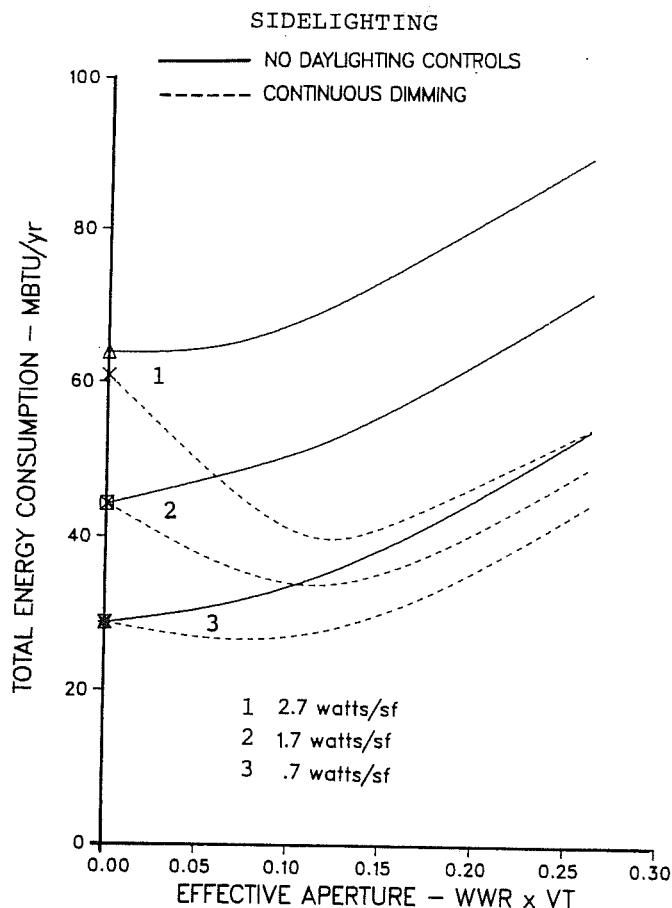2 1.7 watts/sf
3 .7 watts/sf

Fig. 10.   DOE-2 prediction of total annual energy consumption vs. effective aperture (window-to-wall ratio times visible transmittance) for a south-facing sidelit office module in Los Angeles, with and without daylighting controls for different lighting power densities.

SKYLIGHTING

NO DAYLIGHTING CONTROLS
CONTINUOUS DIMMING

1 2.7 watts/sf
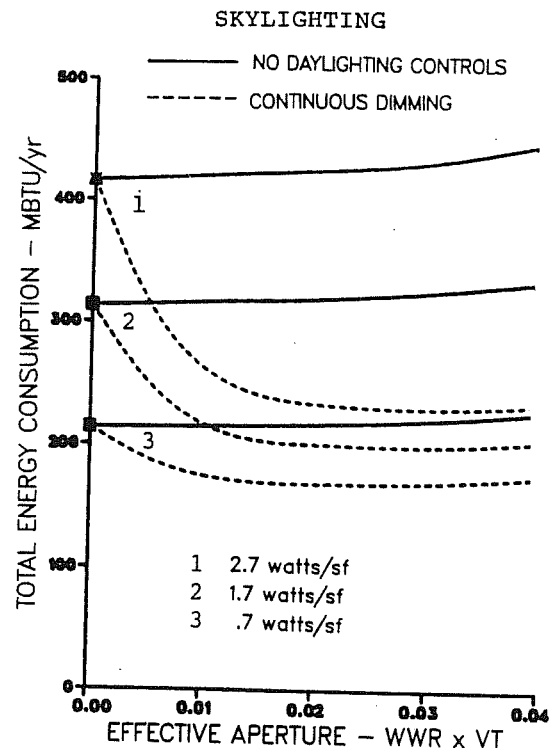2 1.7 watts/sf
3 .7 watts/sf

Fig. 11.   DOE-2 prediction of total annual energy consumption vs. effective aperture (skylight-to-roof ratio times visible transmittance times well factor) for a skylit core module in Los Angeles with and without daylighting controls, for different lighting power densities.

(4) What is the potential of innovative glazing systems? Using functional value input, many types of existing and hypothetical non-conventional glazing can be modeled. For example, Fig. 13 shows sample results of a study comparing four types of glass: conventional clear glass; conventional low-transmittance glass; a hypothetical glass whose transmittance decreases as solar radiation intensity on the glass increases; and hypothetical glass whose transmittance is modulated hour by hour so as to allow only enough light transmission to just meet a 50 fc illuminance setpoint [28].

8. FUTURE DIRECTIONS

The present version of the program (DOE-2.1C) calculates interior illuminance for conventional window designs and simple room geometries using a preprocessor calculation and sun control systems such as shades, drapes, and blinds that are assumed to be ideal diffusers. The program is being expanded to model (1) geometrically complex sunshading solutions, such as louvers and light shelves; (2) designs where internally reflected light is important, such as those with skylights having deep light wells; and (3) unique architectural spaces, such as large atria which provide daylight to adjacent rooms. .

Because direct calculation of interior illuminance from complex sunshading systems is difficult and sometimes impossible, a new coefficient-of-utilization (CU) model is being developed which is based on data calculated or measured outside the DOE-2 program. This

Annual lighting energy (MBtu) / Annual lighting energy (GJ) vs Effective aperture (WWR)(T_v)

No daylighting
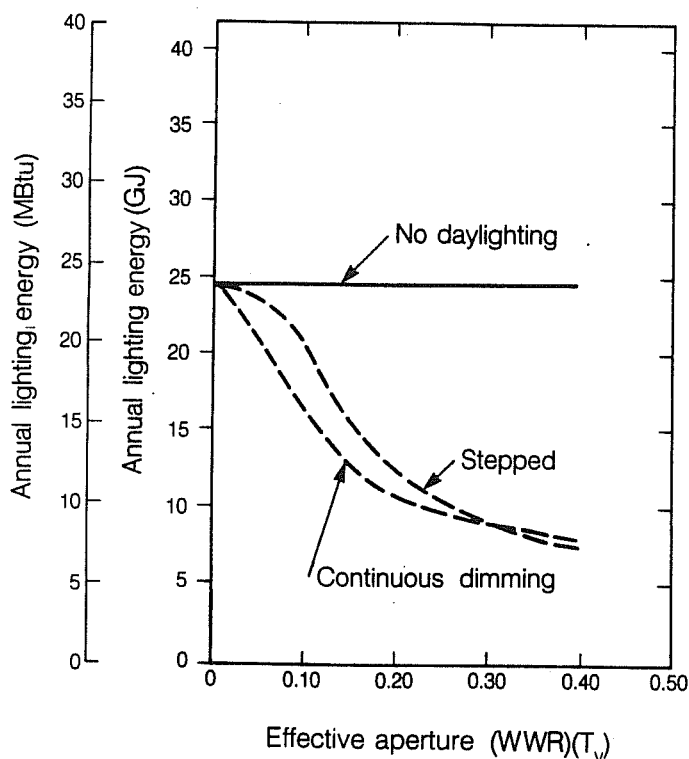Stepped
Continuous dimming

Fig. 12.   DOE-2 Comparison between the effects of stepped switching and continuous dimming on annual electric lighting energy consumption with daylighting for a south-facing sidelit office module in Madison, WI.
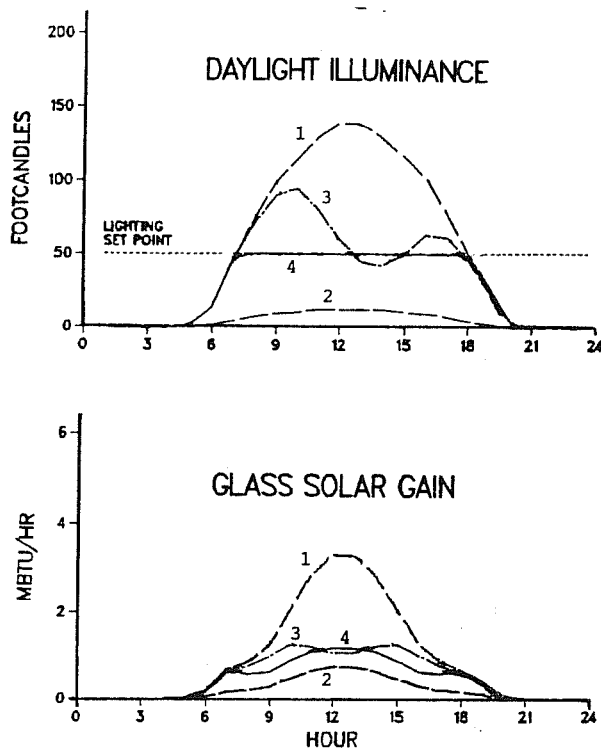
Fig. 13. DOE-2 calculation of daylight illuminance and solar gain in a south-facing sidelit office module for a clear day in Madison, WI. Four different glass types are compared -- (1) conventional, high-transmittance clear glass (VT=78%); (2) conventional, low-transmittance reflective glass (VT=7%); (3) hypothetical photochromic glass whose transmittance decreases from 78% to 20% as incident solar radiation increases; and (4) hypothetical electrochromic glass whose transmittance is modulated hour by hour to just meet a 50 fc illuminance setpoint.

model includes five coefficients that are sensitive to illumination at the window plane from the ground, sky, and sun. It will be implemented in several ways. Some designs, such as flat-louver systems, can be standardized but may be too complex to calculate in DOE-2. The coefficients for these systems would be precalculated by SUPERLITE (using measured angle-dependent luminance data for the shading devices) and stored in a DOE-2 library. To obtain values for specific products rather than for generic designs, SUPERLITE could be used as a preprocessor to DOE-2, generating the specific coefficients directly.

A second category includes daylighting systems, such as curved semi-specular light shelves, that can be standardized but may be too complex to calculate using existing computational models. In this instance, the required illuminance data would be generated from scale models in the LBL sky simulator under a full range of overcast, clear-sky, and direct-sun conditions. Results would be converted to coefficients and stored in the DOE-2 library.

A third category includes unique designs which will not be found in the DOE-2 library. In this case, a user could develop the required data from model studies, convert these data into a format compatible with the CU calculation, and input the results into the program library. Each user could thus create a personal library of custom designs for evaluation.

A parallel effort is underway to expand the capability of DOE-2 to simulate conduction and solar heat gain through windows with shading devices. Coordinated libraries of solar heat gain coefficients and CU's will allow the program to accurately simulate the hour-by-hour thermal behavior of complex designs at the same time as interior daylight illuminance is calculated.

Finally, the algorithms used for daylight availability, particularly for overcast and partly-cloudy conditions, and for discomfort glare will be upgraded as new data in these areas become available.

We are thus working towards an energy model that has a high degree of flexibility and should be responsive to the latest in architectural design strategies.

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